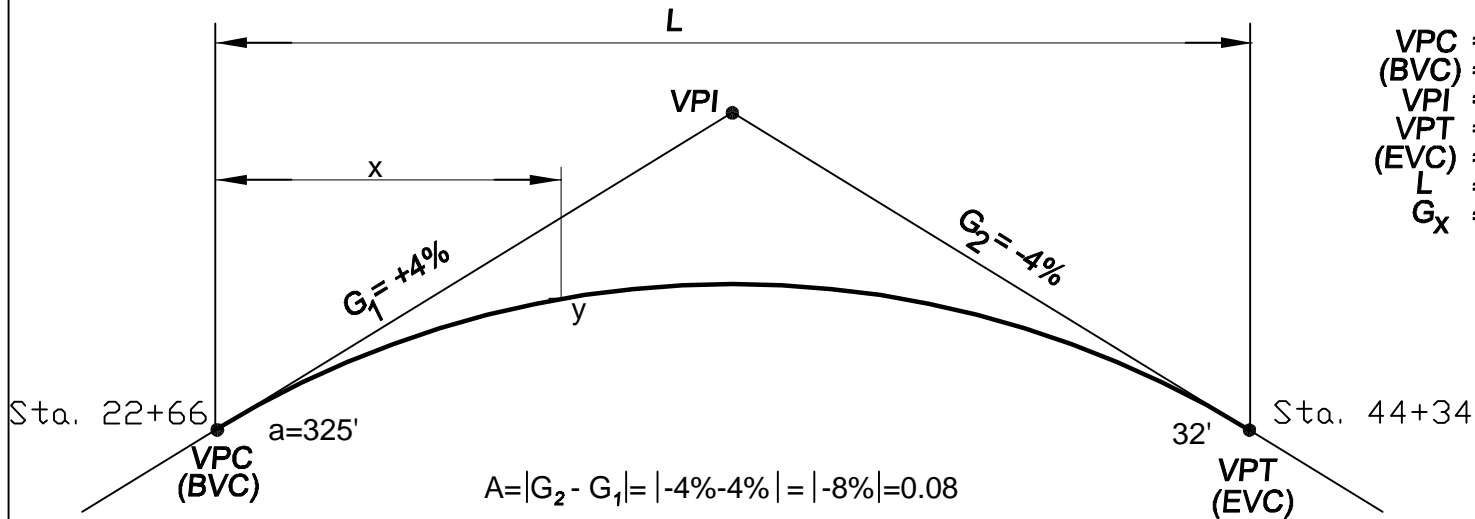


7.1

GEOMETRY OF A (CREST) VERTICAL CURVE



- VPC = Vertical Point of Curvature
- (BVC) = Begin Vertical Curve
- VPI = Vertical Point of Intersection
- VPT = Vertical Point of Tangency
- (EVC) = End Vertical Curve
- L = Length of the curve
- G_x = Slope

$$A = |G_2 - G_1| = |-4\% - 4\%| = |-8\%| = 0.08$$

$$L = (44+34) - (22+66)$$

$$L = 4434 - 2266$$

$$L = 2168 \text{ feet}$$

$$\text{EQ. (7.5): } X_{HI} = L \cdot \frac{G_1}{G_1 - G_2} = 2168 \frac{4\%}{4\% - (-4\%)} = 2168 \frac{0.04}{0.08} = 1084 \text{ feet}$$

$$\text{EQ. (7.4): } c = \frac{G_2 - G_1}{2L} = \frac{-0.08}{2(2168)} = -0.0000185/\text{ft}$$

EQ. (7.3):

$$y = a + bx + cx^2$$

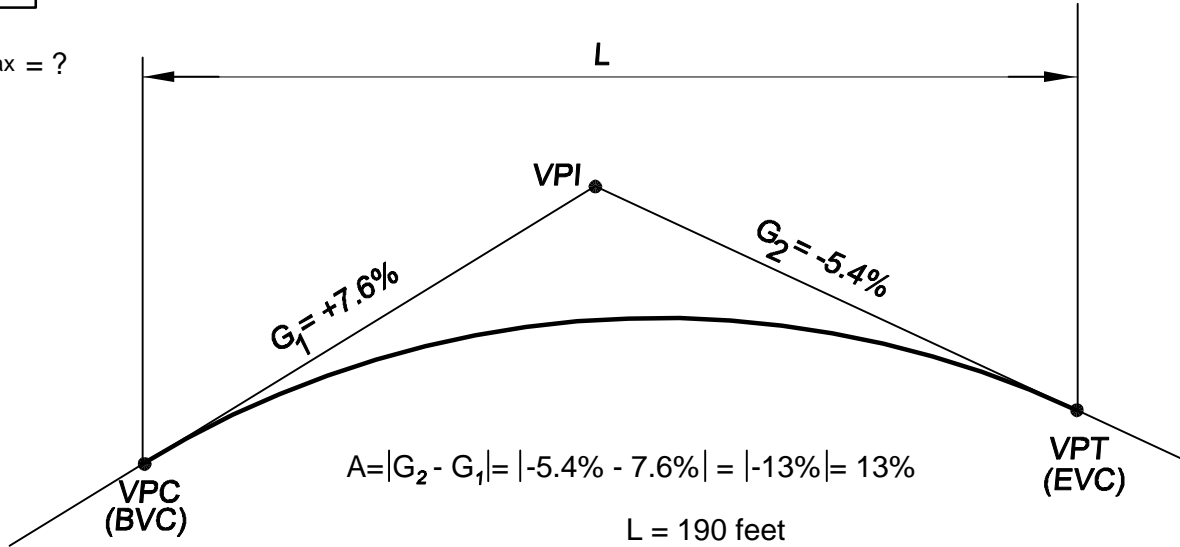
$$y = 325 \text{ ft.} + 0.04(1084 \text{ ft.}) + (-0.0000185/\text{ft})(1084 \text{ ft.})^2$$

$$y = 325 + 43.4 - 21.7 = \underline{346.7 \text{ ft.}}$$

7.7

SSD ON A CREST VERTICAL CURVE

$S_{Max} = ?$



- VPC = Vertical Point of Curvature
- (BVC) = Begin Vertical Curve
- VPI = Vertical Point of Intersection
- VPT = Vertical Point of Tangency
- (EVC) = End Vertical Curve
- L = Length of the curve
- G_x = Slope

$L = 190$ feet

Figure 7.13

$h_1 = 3.5'$
 $h_2 = 2.0'$

Standard h_1 and h_2

$S_{Max} = ?$

SSD < L

(EQ. 7.17) $L_{Min 1} = \frac{A \times SSD^2}{2158}$

$190 = \frac{13.0 \times SSD^2}{2158}$

SSD_{ACTUAL PROVIDED} = 177.6 feet

Table 7.4

~~$S = 30\text{mph} \Rightarrow 200 \text{ feet} = SSD_{NEEDED}$~~

$S = 25\text{mph} \Rightarrow 155 \text{ feet} = SSD_{NEEDED}$ ✓

EQUATIONS ASSUME

~~SSD > L~~

~~$L_{Min 2} = 2SSD - \frac{2158}{A}$ (EQ. 7.17)~~

~~$190 = 2SSD - \frac{2158}{13}$~~

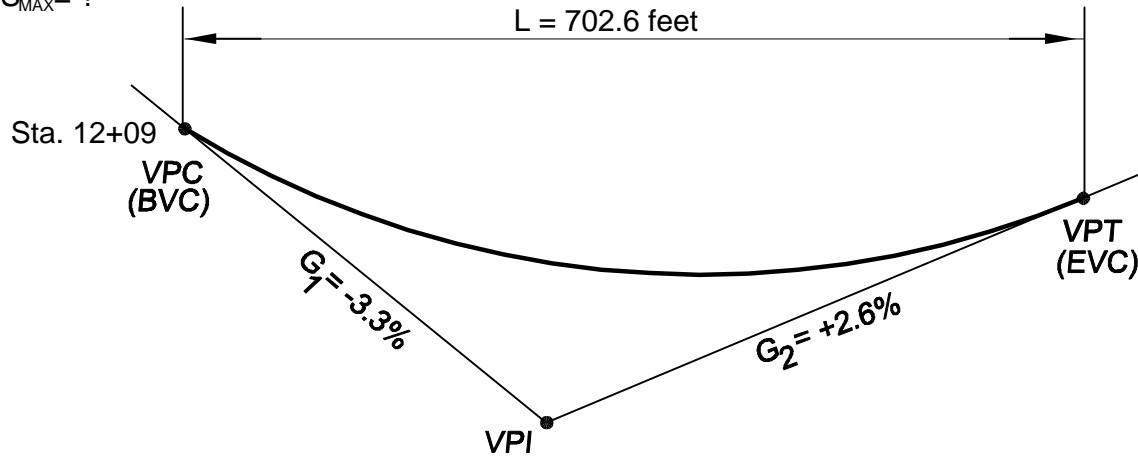
~~SSD = 178.0 feet~~

If not using Standard h_1 & h_2 then use (EQ. 7.16) not (EQ. 7.17)

7.11

SSD ON A SAG VERTICAL CURVE

S_{MAX} = ?



- VPC = Vertical Point of Curvature
- (BVC) = Begin Vertical Curve
- VPI = Vertical Point of Intersection
- VPT = Vertical Point of Tangency
- (EVC) = End Vertical Curve
- L = Length of the curve
- G_x = Slope

$$A = |G_1 - G_2| = |-3.3\% - 2.6\%| = |-5.9\%| = 5.9\%$$

SSD_{ACTUAL}
S = ?

SSD < L

$$L_{Min 1} = \frac{|A| S^2}{200(2+0.017455S)} \quad \text{(EQ. 7.18)}$$

$$702.6 = \frac{5.9 S^2}{200(2+0.017455S)}$$

$$23816.9 = \frac{S^2}{2+0.017453S}$$

$$47633.9 + 415.7S - S^2 = 0$$

$$0 = S^2 - 415.7S - 47633.9$$

$$\frac{-(-415.7) \pm \sqrt{(-415.7)^2 - 4(1)(-47633.9)}}{2(1)} \quad \text{(Quadratic Equation)}$$

$$\frac{-(-415.7) \pm \sqrt{(-415.7)^2 - 4(1)(-47633.9)}}{2(1)} = \frac{-(-415.7) \pm \sqrt{172848 + 190576}}{2(1)} \Rightarrow \text{SSD}_{ACTUAL PROVIDED} = \frac{416 \pm 603}{2} = 510 \quad \cancel{43.5}$$

Table 7.4

S = 55mph ⇒ 495 feet ✓

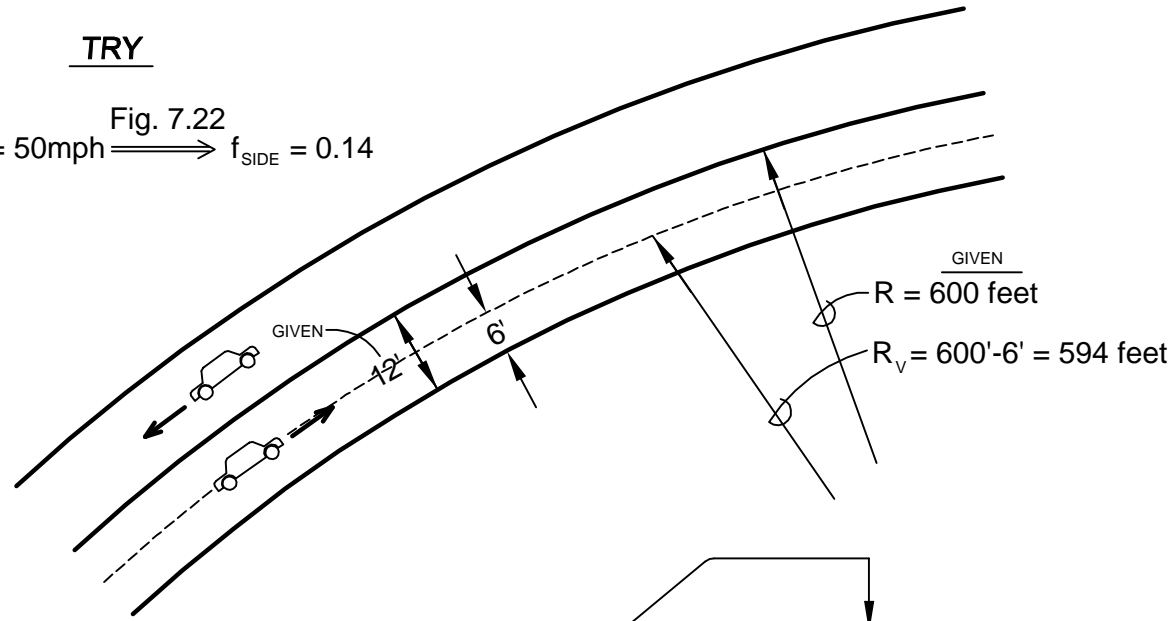
S = 60mph ⇒ 570 feet

7.22

SUPERELEVATION

S = ?

TRY
 Fig. 7.22
 $S_{DESIGN} = 50\text{mph} \implies f_{SIDE} = 0.14$



ft. $R_v = \frac{V^2}{g(e + f_{SIDE})}$ EQ. (7.24)

$594 \text{ ft} = \frac{(50\text{mph} \times 1.477)^2}{32.2 \text{ ft/sec/sec}(e + 0.14)}$

$3.5566 = \frac{1}{e + 0.14}$

$3.56e + 0.498 = 1$

$3.56e = 0.502$

$e = 0.14 \text{ ft/ft}$

Too High "e"
 (See Fig. 7.23)

TRY
 $S_{DESIGN} = 40\text{mph} \implies f_{SIDE} = 0.15$

$594 \text{ ft} = \frac{(40\text{mph} \times 1.477)^2}{32.2 \text{ ft/sec/sec}(e + 0.15)}$

$5.56 = \frac{1}{e + 0.15}$

$5.56 e + 0.833 = 1$

$5.56 e = 0.167$

$e = 0.03 \text{ ft/ft}$

Too Low "e"

$S_{DESIGN} = 45\text{mph} \implies 594 = \frac{(45 \times 1.477)^2}{32.2(e + 0.15)}$

$S_{POSTED} = S_{DESIGN} - 5 = 40\text{mph}$

$e = 0.08 \checkmark \text{O.K.}$

7.18

SSD ON A HORIZONTAL CURVE

$M_s = ?$

$T = 32+50 - 28+00 = 4+50 = 450'$

$T = R \tan \frac{\Delta}{2}$

$450 \text{ ft} = (1650 \text{ ft}) \tan \frac{\Delta}{2}$

$\tan^{-1}(0.2727) = \frac{\Delta}{2}$

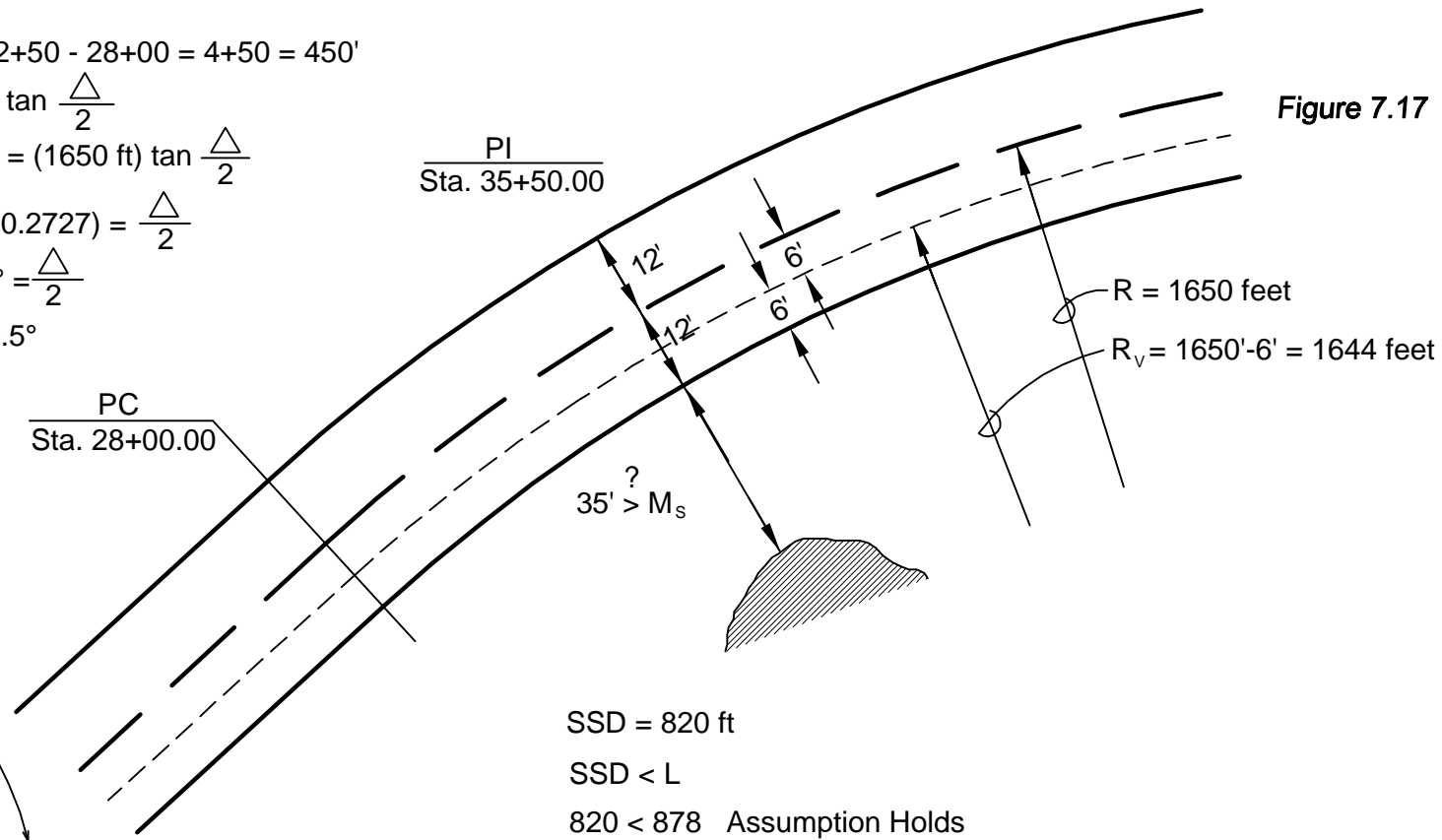
$15.25^\circ = \frac{\Delta}{2}$

$\Delta = 30.5^\circ$

PC
Sta. 28+00.00

PI
Sta. 35+50.00

Figure 7.17



SSD = 820 ft
 SSD < L
 820 < 878 Assumption Holds

$L = \frac{100 \Delta}{D} = \frac{100(30.5)}{3.472} = 878 \text{ ft}$

$D = \frac{5729.6}{R} = \frac{5729.6}{1650} = 3.472$

Assume SSD < L

$SSD = \frac{\pi \times R_v}{90} (\cos^{-1} \frac{R_v - M_s}{R_v})$

$820 = \frac{(3.1415)(1644)}{90} \cos^{-1}(\frac{1644 - M_s}{1644})$

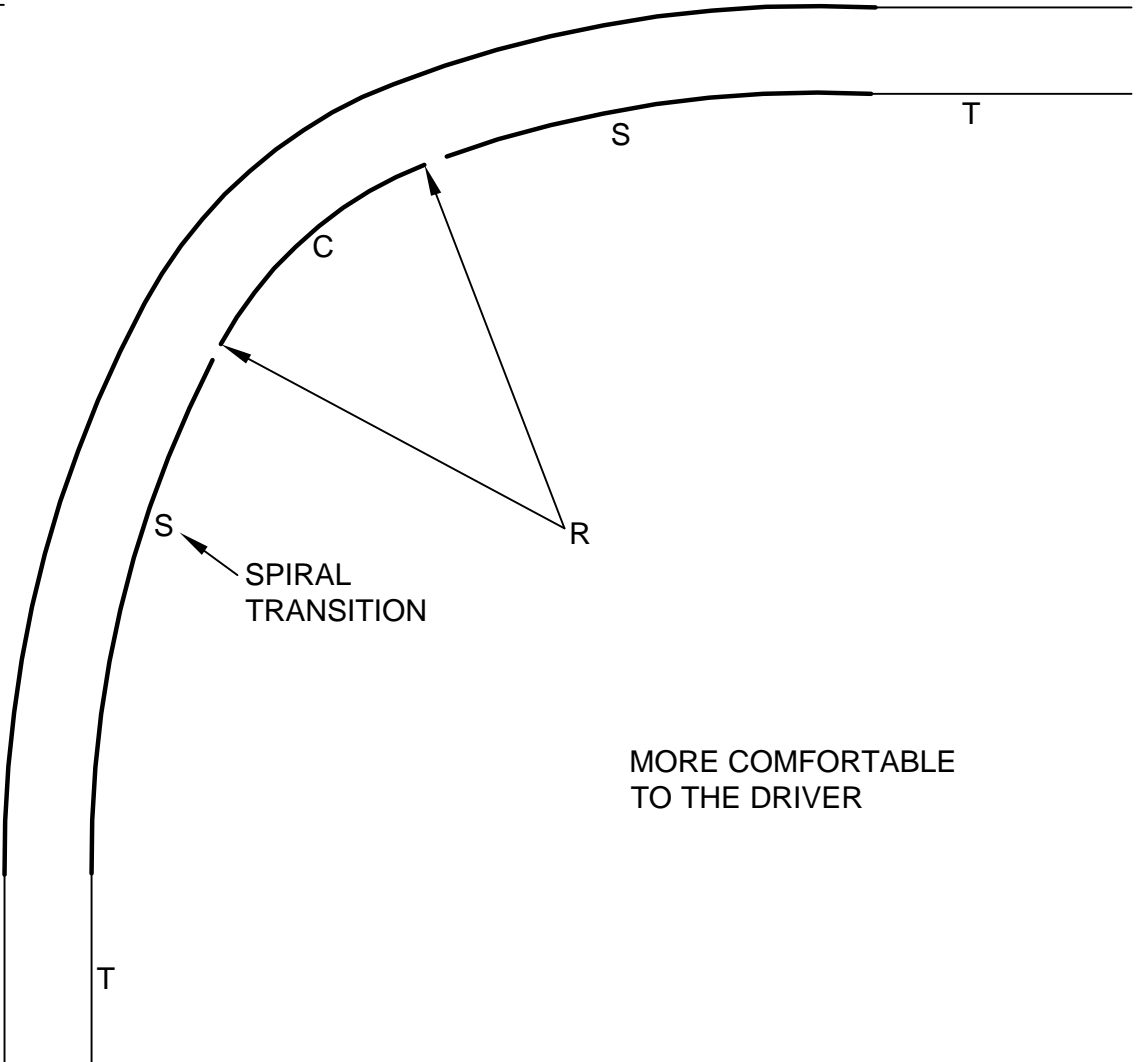
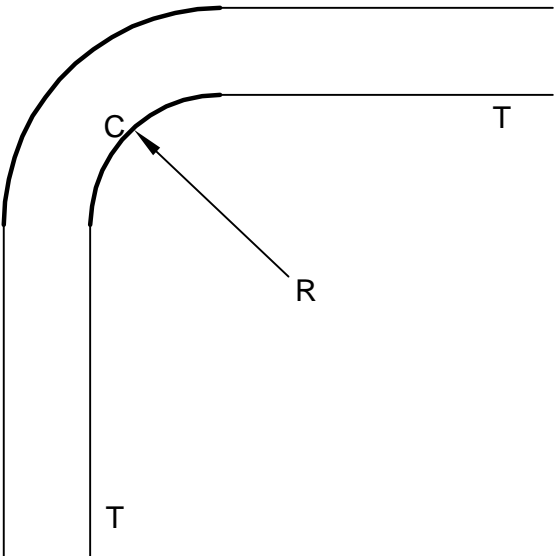
$\cos^{-1}(\frac{1644 - M_s}{1644}) = 14.2895 \Rightarrow \frac{1644 - M_s}{1644} = 0.969 \Rightarrow M_s = \underline{\underline{50.9 \text{ ft.}}}$

THEREFORE SET-BACK
 NEEDED OF:

$50.9 - 35 = \underline{\underline{15.9 \text{ ft.}}}$

USE OF SPIRAL CURVES

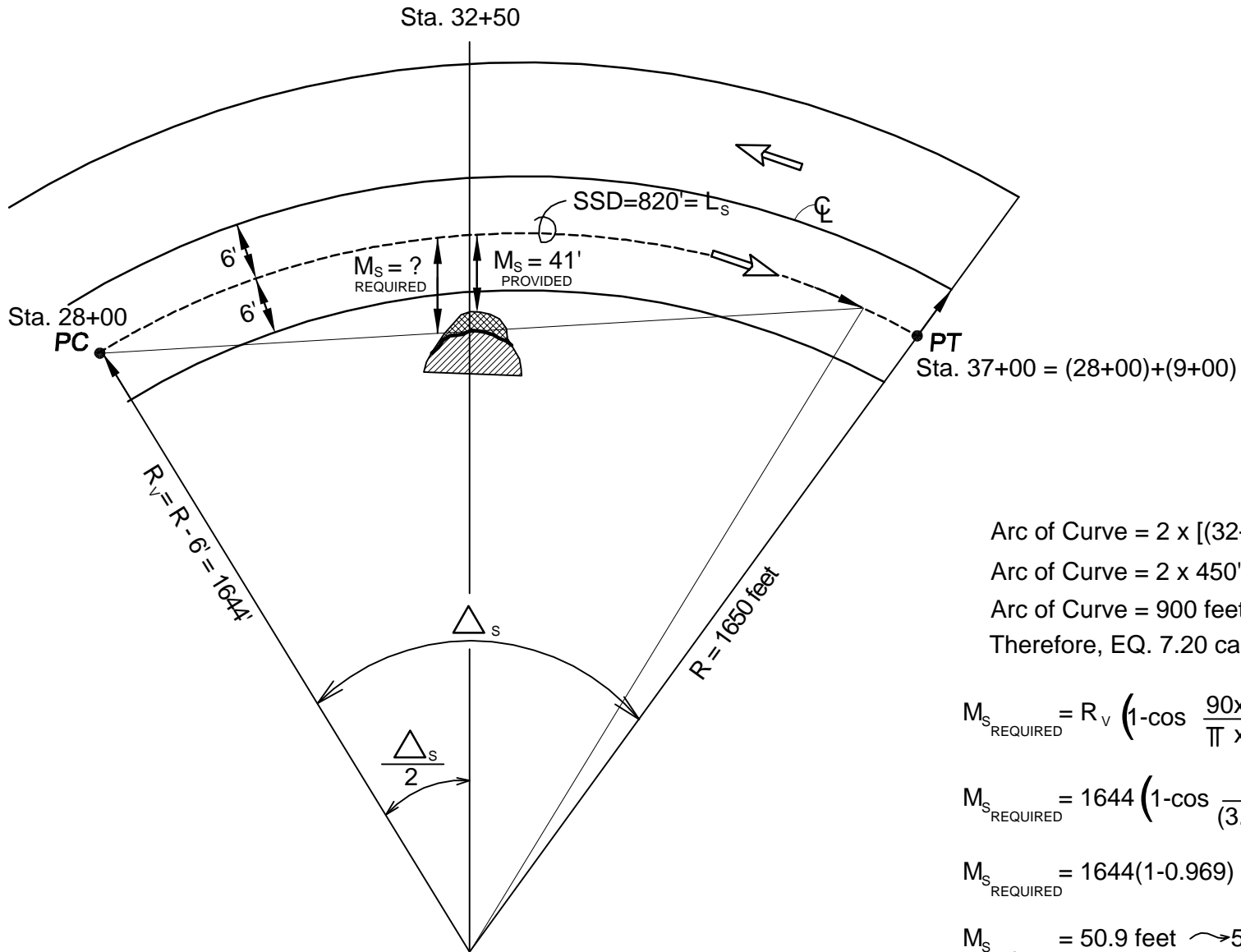
NO SPIRAL
TRANSITION



T = Tangent Section (Straight)
C = Circular Curve

MORE COMFORTABLE
TO THE DRIVER

SSD ON A HORIZONTAL CURVE



$$\text{Arc of Curve} = 2 \times [(32+50) - (28+00)]$$

$$\text{Arc of Curve} = 2 \times 450' = 900 \text{ feet}$$

$$\text{Arc of Curve} = 900 \text{ feet} > \text{SSD} = 820 \text{ feet}$$

Therefore, EQ. 7.20 can be used

$$M_{s_{\text{REQUIRED}}} = R_v \left(1 - \cos \frac{90 \times \text{SSD}}{\pi \times R_v} \right) \text{ (EQ. 7.20)}$$

$$M_{s_{\text{REQUIRED}}} = 1644 \left(1 - \cos \frac{90 \times 820}{(3.1416)(1644)} \right)$$

$$M_{s_{\text{REQUIRED}}} = 1644(1 - 0.969)$$

$$M_{s_{\text{REQUIRED}}} = 50.9 \text{ feet} \rightsquigarrow 51 \text{ feet}$$

Required Cut-Back Distance = $51' - 41' = \underline{10 \text{ feet}}$